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# Sequential high temperature reduction, low temperature hydrolysis for the regeneration of sulfated $NO_x$ trap catalysts

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#### **Abstract**

We describe a new method that minimizes irreversible Pt sintering during the desulfation of sulfated Pt/BaO/Al<sub>2</sub>O<sub>3</sub> lean NO<sub>x</sub> trap (LNT) catalysts. While it is known that the addition of  $H_2O$  to  $H_2$  promotes desulfation, we find that the significant and irreversible Pt sintering arising from the presence of water is unavoidable. Control of precious metal sintering is considered to be one of the critical issues in the development of durable LNT catalysts. The new method described here is a sequential desulfation process: the first step is to reduce the sulfates with hydrogen only at higher temperatures to form BaS, followed by a treatment of the thus reduced sample with water at low to moderate temperatures to convert BaS to BaO and  $H_2S$ . The data showed that Pt sintering was significantly inhibited due to the absence of  $H_2O$  during the desulfation at high temperatures, and also demonstrates the similar  $NO_x$  uptake with the desulfated sample cooperatively with  $H_2$  and  $H_2O$ . This study clearly revealed both positive and negative roles for water in desulfation processes and these factors must be considered when optimizing LNT operation. Published by Elsevier B.V.

Keywords: NOx storage; Pt/BaO/Al2O3; Desulfation; Pt sintering; H2O effect

#### 1. Introduction

The lean  $NO_x$  trap (LNT) technology, also known as  $NO_x$  adsorber and  $NO_x$  storage/reduction, is considered one of the promising solutions to reduce  $NO_x$  emissions from lean burn gasoline and diesel engines [1,2]. Typically, a LNT catalyst, which consists of a precious metal (e.g., Pt), a storage material (alkali and/or alkaline earth oxides, e.g., BaO), and a high surface area support material (usually  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>), operates under transient conditions. During the lean cycle, NO is oxidized to  $NO_2$  over Pt sites and the  $NO_2$  reacts with BaO/Ba(OH)<sub>2</sub>/BaCO<sub>3</sub> species to be stored as Ba( $NO_3$ )<sub>2</sub>, which is subsequently reduced to  $N_2$  by reductants during a short rich cycle.

Although there has been significant progress in the development of high performance  $NO_x$  storage catalysts, the stability of the material against  $SO_2$  poisoning remains a critical issue. The precious metal component of the catalyst that

converts NO to NO<sub>2</sub> is also effective in the oxidation of SO<sub>2</sub> to SO<sub>3</sub>. Thus, the LNT catalyst is poisoned by SO<sub>2</sub> due to the higher affinity of barium oxide to react with SO<sub>3</sub> than NO<sub>2</sub>, as the BaSO<sub>4</sub> formed is thermodynamically more stable than Ba(NO<sub>3</sub>)<sub>2</sub> [3]. The conversion of BaO into BaSO<sub>4</sub> results in a decrease in the number of available sites for  $NO_x$  adsorption, leading to deactivation of the catalysts. Even low concentrations of SO<sub>2</sub> gradually reduce the ability of the catalyst to store  $NO_x$ . The regeneration process to desulfate the catalysts requires high temperatures (e.g., 600 °C or higher) and a reducing gas (e.g., H<sub>2</sub>). During this process, sulfate species are transformed to sulfides, and the primary S-containing species desorbing is H<sub>2</sub>S [4]. Several research groups have reported [5– 7] that water plays a key role in promoting the desulfation process, enhancing the production of H<sub>2</sub>S when a reductant is introduced together with water.

Water, however, has also been shown to have a negative effect on the catalytic performance as it facilitates the deactivation of the catalyst via the promotion of Pt sintering [8]. In addition, our group has clearly demonstrated that the  $NO_x$  uptake efficiency is adversely affected by the growth of platinum particles arising from thermal aging [9]. Hence, Pt sintering is detrimental to the performance of these LNT

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catalysts. Even more important is the irreversible nature of this deactivation process since the sintered Pt particles cannot be redispersed. To explore ways to prevent such sintering, we studied a desulfation process in which H2 and H2O are separately introduced in two sequential steps: desulfation with H<sub>2</sub> only at high temperatures (up to 800 °C), followed by H<sub>2</sub>O treatment at lower temperatures (maximum of 300 °C). The first step is expected to transform the sulfate species into sulfides and even desorb some of the sulfur as H<sub>2</sub>S, while minimizing the Pt sintering. In the second step, the thus formed BaS reacts with H<sub>2</sub>O in a hydrolysis reaction to form BaO and additional H<sub>2</sub>S. The catalyst desulfated by this two-step process showed very similar NO<sub>x</sub> uptake properties as the one that was desulfated in  $H_2 + H_2O$ ; however, the sintering of the Pt particles was almost completely inhibited. The high Pt dispersion retained after desulfation should positively affect the long-term stability of the catalyst.

# 2. Experimental

Pt–BaO(20)/Al<sub>2</sub>O<sub>3</sub> samples were prepared by using a conventional impregnation method, as described in our previous publication [10]. The samples were calcined at 500 °C for 2 h in flowing air, resulting in 2 wt% Pt and 20 wt% BaO supported on an  $\sim$ 200 m<sup>2</sup>/gm  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>.

The sulfation/desulfation studies were performed in a fixed bed quartz reactor following procedures as illustrated in Fig. 1. Sulfations were carried out by treating 0.3 g of catalyst at 500 °C with 10%  $O_2$  for 2 h, followed by exposure to 50 ppm  $SO_2$  and 10%  $O_2$  balanced with He at 300 °C for 6.5 h. Since we did not observe any breakthrough of  $SO_2$  within the detection limit of 5 ppm  $SO_2$  during sulfation period with a mass spectrometer (MKS, Minilab), it is assumed that all sulfur species are taken up by the samples. Thus, the total amount of  $SO_2$  exposed is 0.24 mmol, which is smaller than the amount of Ba (0.39 mmol) in the sample.

After completing the sulfation process and without exposing the sample to the ambient air,  $H_2$  temperature programmed reaction ( $H_2$  TPRX) either with or without  $H_2$ O was performed. The temperature was ramped from 20 °C (without  $H_2$ O) or 160 °C (with 10%  $H_2$ O) to 800 °C under the 10%  $H_2$  in He flow

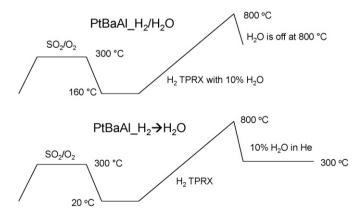


Fig. 1. The two regeneration protocols used here to desulfate the sulfated Pt–BaO(20)/Al<sub>2</sub>O<sub>3</sub> samples.

at a rate of 8 °C/min. For the case of the sequential process, 10%  $H_2O$  in He was subsequently applied to the sample at 300 °C, a temperature that was obtained after completing the  $H_2$  TPRX up to 800 °C. A mass spectrometer was used to observe the evolution of  $H_2S$  during these processes. The samples with simultaneous exposure to  $H_2/H_2O$ , and the sequential process of exposure to  $H_2$  TPRX followed by  $H_2O$  are designated as PtBaAl\_ $H_2/H_2O$  and PtBaAl\_ $H_2 \rightarrow H_2O$ , respectively.

The  $NO_x$  uptake measurements were carried out in the same reactor as the sulfation/desulfation experiments, with detailed reaction conditions described elsewhere [10].  $NO_x$  uptakes are defined as the ratio of the amount of  $NO_x$  stored to the amount of inlet  $NO_x$  (200 ppm) during the lean cycle for 30 min, prior to a rich cycle of 1 min, measured at 300 °C.

TEM images were collected for PtBaAl\_ $H_2/H_2O$  and PtBaAl\_ $H_2 \rightarrow H_2O$  samples. The TEM specimens were prepared by dusting the powder particles onto a carbon film-coated 200 mesh copper TEM grid. TEM analysis was carried out on a JEOL JEM 2010 microscope.

X-ray photoelectron spectroscopy (XPS) experiments were carried out for PtBaAl\_H<sub>2</sub>/H<sub>2</sub>O and PtBaAl\_H<sub>2</sub>  $\rightarrow$  H<sub>2</sub>O samples in the analysis chamber of a Physical Electronics Instruments Quantum 2000, using Al K $\alpha$  X-rays and a pass energy of 71 eV. The position and intensity of the Al 2s peak at 119.2 eV were used as references.

### 3. Results and discussion

Fig. 2 shows the  $H_2$  TPRX spectra obtained during temperature ramping with  $H_2$  (dotted red trace) and  $H_2/H_2O$  (solid black trace) for the sulfated Pt–Ba(20)/Al<sub>2</sub>O<sub>3</sub> samples. Note that the  $H_2S$  signal from the mass spectrometer fluctuated significantly for the case of  $H_2$  TPRX with water, most likely due to the condensation of water along the gas lines which are kept at room temperature.  $H_2S$  evolution, resulting from the

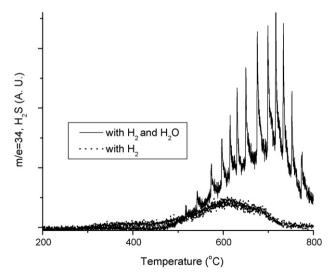


Fig. 2. H<sub>2</sub> TPRX spectra obtained during the two desulfation procedures (i.e., with and without water). The cooperative and sequential treatments are indicated by the solid and dotted line, respectively.

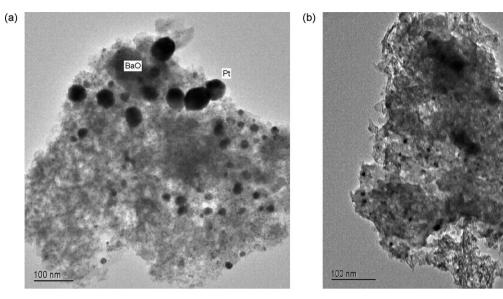


Fig. 3. TEM images of PtBaAl\_ $H_2/H_2O$  (a) and PtBaAl\_ $H_2 \rightarrow H_2O$  (b) samples.

reaction between sulfate and hydrogen and the subsequent hydrolysis reaction between BaS and  $H_2O$  as described in reactions (1) and (2), was observed in both  $H_2$  TPRX spectra.

$$BaSO_4 + 4H_2 \rightarrow BaS + 4H_2O \tag{1}$$

$$BaS + H_2O \rightarrow BaO + H_2S \tag{2}$$

For the case of regeneration with hydrogen only, the amount of H<sub>2</sub>S evolved is about four times less than that observed with H<sub>2</sub>/H<sub>2</sub>O, and the peak maximum is located at 600 °C. On the basis of our prior time-resolved X-ray diffraction (TR-XRD) results [4], BaSO<sub>4</sub> is transformed into a BaS phase just above 550 °C, with the BaS continuing to grow up to 800 °C, concurrent with the generation of H<sub>2</sub>S during the temperature ramping. The lesser amount of H<sub>2</sub>S evolution observed in the H<sub>2</sub>-only process is due to the limited availability of H<sub>2</sub>O (only a small amount of water, formed during sulfate reduction, can participate in the subsequent hydrolysis of BaS). On the other hand, regeneration with H<sub>2</sub>/H<sub>2</sub>O gives rise to a larger amount of H<sub>2</sub>S peaked at higher temperature, i.e., 700 °C. In the presence of water, the hydrolysis reaction (2) becomes facile since a sufficient amount of water is available to hydrolyze the BaS formed in the reduction portion of the desulfation process. Therefore, the effect of H<sub>2</sub>O on H<sub>2</sub>S evolution becomes significant above 550 °C, where BaS begins to form, leading to the formation of additional H<sub>2</sub>S from reaction (2) between BaS and H<sub>2</sub>O at temperatures higher than 550 °C.

In summary, water is quite effective in removing residual sulfur species on the LNT catalyst samples via its reaction with barium sulfide. The process restores the  $NO_x$  storage capacity of the LNT system, in agreement with findings of other researchers [5–7] who reported the promotional effect of  $H_2O$  during desulfation processes.

One of the critical issues for maintaining LNT performance, as we have already mentioned above, is the sintering of metallic Pt particles during high temperature (up to 800 °C) desulfation. In other work, Graham et al. [11] reported that the average Pt

particle size in Pt/Al<sub>2</sub>O<sub>3</sub> samples ranges from 2 to 6 nm after treatment in a H<sub>2</sub> flow up to 950 °C. In addition, we [9] have shown that the average Pt particle size does not exceed 10 nm after a model Pt-Ba/Al<sub>2</sub>O<sub>3</sub> catalyst is treated in H<sub>2</sub> flow up to 900 °C (note that the sample is different from that in the current study). However, as the TEM image in panel (a) of Fig. 3 clearly demonstrates, Pt particle sizes increased to about 10-30 nm (some Pt clusters are even over 50 nm) during H<sub>2</sub> TPRX up to  $800~^{\circ}\text{C}$  in the presence of  $10\%~\text{H}_2\text{O}$ . Note also the virtual absence of Pt particles smaller than 10 nm in this catalyst. These results are in good agreement with those of Barbier and Duprez [8] that revealed accelerated sintering of platinum particles in the presence of H<sub>2</sub>O under both oxidizing or reducing conditions at temperatures higher than 550 °C. They concluded that steam apparently increased the rate constant of the Pt sintering reaction [8].

Meanwhile, a prior study published by our group [9] clearly demonstrates the inverse relationship between Pt particle size and  $NO_x$  storage performance. In this study, we used the results of a combined TR-XRD and  $NO_x$  uptake study to establish a direct correlation between catalyst performance and Pt particle size as a function of sample aging temperature and time. The relationship suggests that retention of Pt particle size during regeneration processes at high temperatures is crucial to maintaining high  $NO_x$  storage/reduction performance. In fact, the sintering of Pt particles has a negative effect on the desulfation process as well since they provide the active sites for activating the reductant,  $H_2$ , before it can react with the sulfur-containing species (i.e., barium sulfate).

According to the protocol described in Fig. 1, we separated the simultaneous reduction/hydrolysis process into two sequential steps:  $H_2$  treatment to transform  $BaSO_4$  to BaS (reduction, reaction (1)), followed by subsequent  $H_2O$  treatment at lower temperature (hydrolysis, reaction (2)). This desulfation approach was expected to minimize Pt sintering which occurs extensively at high temperatures in the presence of  $H_2O$ . After reduction in  $H_2$  only up to  $800\ ^{\circ}C$  in the TPRX

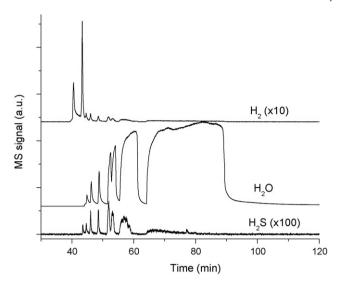


Fig. 4. Gases (H<sub>2</sub>, H<sub>2</sub>O and H<sub>2</sub>S) evolved during H<sub>2</sub>O treatment at 300  $^{\circ}$ C, subsequent to an H<sub>2</sub>-only TPRX up to 800  $^{\circ}$ C.

experiment, the sample was cooled to 300 °C, and then exposed to a 10% H<sub>2</sub>O in He flow (this water concentration is typical in diesel engine exhausts).

Fig. 4 shows mass spectra data of gases  $(H_2O, H_2S)$  and  $H_2$ evolved during H<sub>2</sub>O treatment of the H<sub>2</sub>-reduced sample at 300 °C. Initially, hydrogen is formed just before H<sub>2</sub>O breakthrough via a process (perhaps artifactual) we do not understand at present. As water appears in the effluent, H<sub>2</sub>S evolution is also observed. It is important to note that the possibility of reaction (1) between the H<sub>2</sub> evolved and the residual sulfate species can be excluded since 300 °C is too low of a temperature to generate H<sub>2</sub>S even if the H<sub>2</sub> concentration was significantly higher than present in these experiments. Therefore, H<sub>2</sub>S formed under the conditions used here is explicitly generated via reaction (2) between BaS and H<sub>2</sub>O. Estimating the total amount of H<sub>2</sub>S evolved in this sequential reduction-hydrolysis process reveals that it is only about half of that measured in the regeneration process carried out with simultaneous H<sub>2</sub>/H<sub>2</sub>O flow. The amounts of residual sulfur were also estimated for these two samples with XPS by integrating the S 2p region normalized with the Al 2s region. Consistent with the H<sub>2</sub>S evolution results during H<sub>2</sub> TPRX, the relative surface concentration of S/Al on the PtBaAl\_ $H_2 \rightarrow H_2O$  sample by XPS (2.36%) was found to be about 20% larger than that over the PtBaAl\_H<sub>2</sub>/H<sub>2</sub>O catalyst (1.97%). These results suggest a relatively poorer effectiveness of sulfur removal from these sulfated catalysts using the two-step approach. On the other hand, considering the changes in the average size of the Pt clusters, the sequential treatment resulted in significantly lower Pt particle size increases, as shown in Fig. 3(b). This TEM image clearly demonstrates that the average Pt particle size was between 5 and 10 nm when the sequential desulfation process was applied, while increasing to 10-30 nm (and even to as high as over 50 nm) in the cooperative desulfation process. These results imply that the subsequent H<sub>2</sub>O treatment at 300 °C (following the reduction in H<sub>2</sub> at 800 °C) does not facilitate

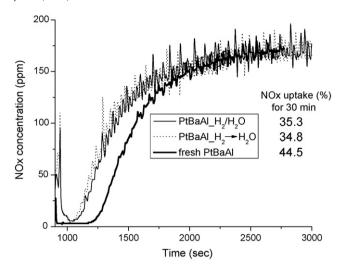


Fig. 5. NO<sub>x</sub> uptake profiles of fresh PtBaAl, PtBaAl\_ $H_2 \rightarrow H_2O$  and PtBaAl\_ $H_2/H_2O$  samples measured at 300 °C.

Pt sintering, only the removal of additional residual sulfurcontaining species.

Fig. 5 shows the  $NO_x$  uptake profiles of fresh Pt–BaO/Al $_2O_3$ , PtBaAl $_1H_2 \rightarrow H_2O$  and PtBaAl $_1H_2/H_2O$  at 300 °C for a 30 min lean period where the inlet  $NO_x$  (NO) concentration was 200 ppm. Surprisingly, no significant difference, either in the total 30 min  $NO_x$  uptake or the region where the full  $NO_x$  uptake occurred, was observed for these samples desulfated by the two different methods (i.e., under simultaneous  $H_2 + H_2O$  flow at 800 °C, or  $H_2$  reduction at 800 °C followed by hydrolysis with  $H_2O$  at 300 °C). Despite the large differences in both the amount of residual S-containing species and the average Pt particle sizes after desulfation by the two protocols, the  $NO_x$  storage properties of the two samples are practically identical. This is thought to be due to a relative cancellation of the effects of these two deactivating phenomena in this particular case.

Although the amount of H<sub>2</sub>S desorbed during the cooperative desulfation process is larger than that of sequential one under the experimental conditions presented here, a modification of the two-step desulfation protocol may offer a means to improve the desulfation efficiency while maintaining the lack of Pt particle size growth. This can be achieved by optimizing the experimental conditions, in particular H<sub>2</sub>O concentration and hydrolysis temperature. Our most recent results [12] suggest that the hydrolysis rate of BaS is significantly enhanced at catalyst temperatures below 120 °C. Therefore, we believe that reacting sulfate to sulfide via reduction in H<sub>2</sub> at high temperatures, and the subsequent hydrolysis of the BaS to BaO in H<sub>2</sub>O at low temperatures (<100 °C), will yield optimum desulfation conditions that result in high levels of sulfur removal (low residual sulfur content). At the same time, this process can ensure the retention of high dispersion levels of Pt particles (small extent of sintering). Both issues are critical for the development of efficient LNT systems: low residual sulfur to preserve high NO<sub>x</sub> storage capacity, and high Pt dispersions to retain high

efficiencies of the precious metal for NO oxidation and  $NO_x$  reduction reactions. Another possible strategy to enhance LNT durability from the findings presented here would be to develop a material specifically designed to stabilize Pt particle size in the presence of  $H_2O$  at elevated temperatures.

#### 4. Conclusions

Desulfation processes of model LNT catalysts are shown to be primarily composed of two elementary reactions, including BaSO<sub>4</sub> reduction to BaS by H<sub>2</sub>, and BaS conversion to BaO and H<sub>2</sub>S by reaction with H<sub>2</sub>O. The second process is regarded as a key factor for promoting irreversible Pt sintering behavior. The idea presented in this contribution is the separation of these two reactions. We reduced BaSO<sub>4</sub> to BaS first at high temperatures with H<sub>2</sub> only, and then performed a reaction with water at much lower temperatures (e.g., 300 °C). The second reaction is known to occur even at room temperature with a sufficient amount of water. By using this sequential desulfation process, we can significantly decrease the levels of Pt sintering. The NO<sub>x</sub> uptake results showed similar NO<sub>x</sub> uptake performance for catalysts desulfated cooperatively with H2 and H2O or sequentially. Our study confirms two important roles of water in desulfation processes, which act on the performance of LNT catalysts in opposite ways. Hence, these findings should be useful for the development of more durable LNT catalysts.

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